

21
9/5/20

Hydraulics

3rd Year civil

First Term (2009 - 2010)

Chapter ()

المراجعة النظرية
كاملة

مراجعة نظري

كاملة

Compare Between Each Of:

1. Manning and Chezy Eqs.,
2. Effect of vegetation and roughness on Manning Coeff.,
3. Effect of curvature with large and small radius on Manning Coeff.,
4. Canal and flume,
5. Chute and drops,
6. Shallow wide sec. and narrow deep sec.,
7. Efficient sec. and economic sec.,
8. Laminar and turbulent flow,
9. Rapidly varied flow and gradually varied flow,
10. Average normal velocity and shear velocity,
11. IR , and IR ,
12. Actual shear stress and critical shear stress,
13. A , R , Y , Y_h and Z ,
14. Specific energy and total energy,
15. Velocity correction factor and momentum correction factor,
16. Alternative depths and conjugate depths,
17. Specific energy, Specific discharge and Specific force diagrams,
18. Critical, sub-critical and super-critical flow,
19. Ideal and Elastic fluids,
20. Newtonian and Non-Newtonian fluids,
21. Stream line, Streak line, Path line and stream tube,
22. Open channel flow and Pipe flow,
23. Steady and Unsteady flow,
24. Uniform and Non-uniform,
25. Effect of viscosity and effect of gravity,
26. Geometric, kinematics and dynamic similarity,
27. Permissible and critical tractive forces,
28. Dimensionally and non-dimensionally homogeneous,
29. Hydraulically smooth and Hydraulically rough surface and
30. the bed canal slopes.

بِسْمِ اللَّهِ الرَّحْمَنِ الرَّحِيمِ

Manning eqn.

$$Q = \frac{1}{n} \cdot \frac{A^{5/3}}{P^{2/3}} \cdot S^{1/2}$$

$$V = \frac{1}{n} \cdot R^{2/3} \cdot S^{1/2}$$

chezy eqn.

$$Q = C \cdot A \cdot \sqrt{R \cdot S} \quad \text{البيوت}$$

$$V = C \cdot \sqrt{R \cdot S} \quad \text{السرعة}$$

Effect of Vegetation

تستخدم (n) في معادله ماننج

$$V \cdot R = \frac{1}{N} \cdot R^{2/3} \cdot S^{1/2}$$

Effect of Roughness

تستخدم (n) في معادله ماننج

$$Q = \frac{1}{n} \cdot \frac{A^{5/3}}{P^{2/3}} \cdot S^{1/2}$$

ملاحظة

زيادة معامل الخشونة للمادة تزيد (n)
زيادة نظام الجريان داخل القناة تزيد (N)

Curve with large radius

زيادة نصف قطر دوران الجريان
تقل معامل ماننج (n)

Curve with small radius

- انخفاض نصف قطر دوران الجريان
(استخدام منحنيات حادة)
يزداد معامل ماننج

Canal

قناة حديدية

Flume

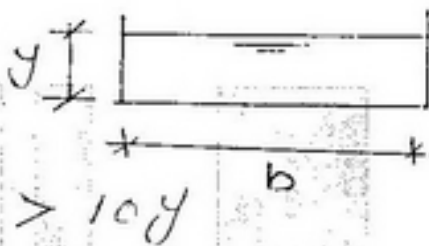
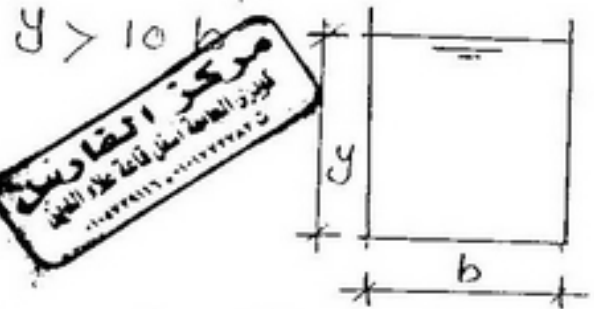
قناة تستخدم في الجمل

Chute

قناة ذات ميل حاد جداً
وقد يكون نسبياً

Drop

انخفاض مفاجئ في قاع القناة
في منطقة ما .

Shallow wideNarrow deepEfficient section

هو المقطاع الذي يعطي أقصى
تدفق ممكن.

Economic section

هو المقطاع الذي يعطي أقل
كميات من مواد البناء وتبطين.

Laminar Flow

حالة السريان عندما تكون
رقم رينولدز
 $Re < 500$

Turbulent flow

حالة السريان عندما تكون
 $Re > 2000$

Rapidly varied flow

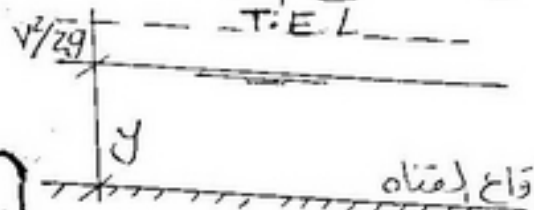
هو السريان الذي يتغير عمقه
بصورة سريعة مع مسافة أفقية
صغيرة.

Gradually varied flow

هو السريان الذي يتغير عمقه
تدريجياً على مسافة أفقية
كبيرة نسبياً.

4 Specific energy

هو كمية الطاقة لكل وحدة
القطاع على المتبار M مستوى
القياس قاع القناة



$$E = y + \frac{v^2}{2g}$$

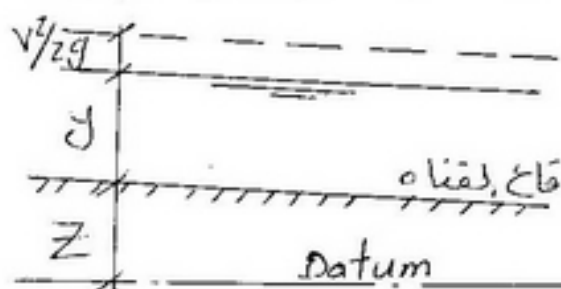
Energy Correction Factor

هو معامل تصحيح قيمة السرعة
داخل معادله الطاقة (α)

$$E = y + \frac{\alpha v^2}{2g}$$

Total Energy

هو كمية الطاقة لكل وحدة داخل لقناة
مقاسه من مستوى قياسي



$$E = Z + y + \frac{v^2}{2g}$$

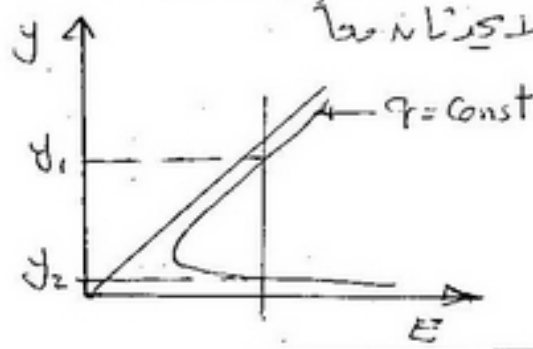
Momentum Correction Factor

هو معامل تصحيح السرعة داخل
معادله كمية الحركة (β)

$$M = \rho Q \beta v$$

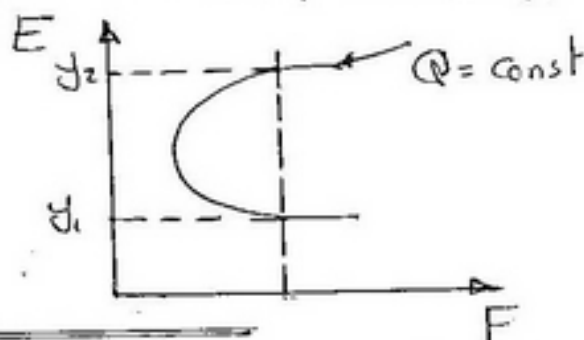
Alternative Depths

هما العمقان اللذان لهما نفس
الطاقة النوعية داخل القطاع
عند ثبات الشرف ولكن أحدهما
subcritical والآخر super critical



Conjugate Depths

هما العمقان اللذان لهما نفس قيمة
السرعة النوعية داخل القطاع عند
ثبات الشرف ولكن أحدهما
subcritical والآخر super critical



| Critical Flow | sub critical flow | super Critical flow |
|----------------------------|----------------------------|----------------------------|
| حاله، لسيان عندما يكون فيه | حاله، لسيان عندما يكون فيه | حاله، لسيان عندما يكون فيه |
| $Fr = 1.00$ | $Fr < 1$ | $Fr > 1$ |

Ideal Fluid

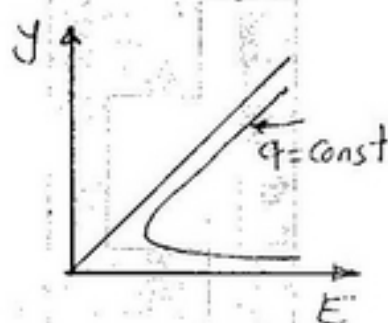
هو المائع الذي ليس له اي مقاومة لغوى، لقص

Elastic Fluid

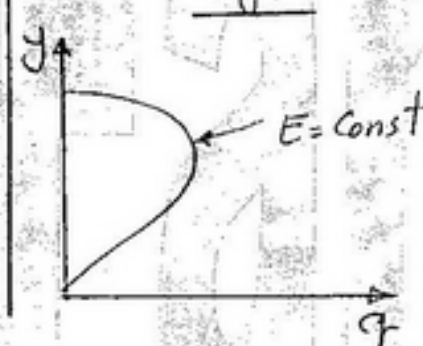
هو المائع الذي له فيه مقاومة عند قوى، لقص دور المكون له تشكل تحت تأثير هذه، لغوى.

مركز الفاس للخدمات الطلابية
استشاري الجامعة
استشاري جامعة علاء الدين
٠١٠٧٢٩١١٦ - ٠١١٢٧٢٧٨١

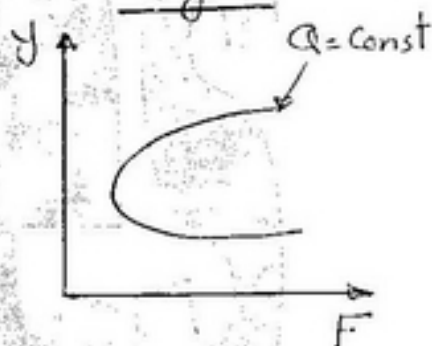
specific energy
Diagram



specific discharge
diagram



specific Force
diagram



Newtonian Fluid

هو المائع الذي لا تتغير لزوجة تبغير الشكل لجادن له

Non - Newtonian Fluid

هو المائع الذي تتغير لزوجة تبغير الشكل لجادن له .

| | | | |
|---|--|--|---|
| 6 <u>Stream Line</u> خطوط والتي تدور حولها شكل السريان والجاس له اتجاه السريان | <u>streak line</u> خط الذي يمر به جميع النقاط التي تمر بنقطة ثابتة | <u>path line</u> خط الذي يمر به جسيم واحد خلال فترة زمنية | <u>stream tube</u> منطقة محددة خطوط السريان التي تقطع شكل السريان |
|---|--|--|---|

open channel Flow

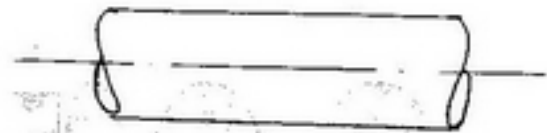
--- T.E.L ---
H.G.L



- ١- متغير المقطع متغير
- ٢- توزيع السرعات متغير
- ٣- ابعاد المقطع متغير
- ٤- سريان تحت تأثير الجاذبية

Pipe Flow

--- T.E.L ---
H.G.L



- ١- متغير المقطع ثابت
- ٢- توزيع السرعات ثابت
- ٣- ابعاد المقطع ثابت
- ٤- سريان تحت تأثير الضغط

Steady Flow

سر سريان الذي لا تتغير خصائصه
تغير الوقت

$$\frac{\partial y}{\partial t} = 0, \quad \frac{\partial v}{\partial t} = 0$$

un steady Flow

سر سريان الذي تتغير خصائصه
مع الوقت

$$\frac{\partial y}{\partial t} \neq 0, \quad \frac{\partial v}{\partial t} \neq 0$$

| <u>Uniform Flow</u> | <u>non-Uniform Flow</u> |
|---|---|
| هو سريان الذي لا تتغير خصائصه مع مسافته . | هو سريان الذي تتغير خصائصه مع مسافته . |
| $\frac{\partial y}{\partial x} = 0$, $\frac{\partial v}{\partial x} = 0$ | $\frac{\partial y}{\partial x} \neq 0$, $\frac{\partial v}{\partial x} \neq 0$ |

| <u>Effect of viscosity</u> | <u>Effect of Gravity</u> |
|----------------------------------|------------------------------------|
| يعتمد تأثير اللزوجة على قيمه R | يعتمد تأثير الجاذبية على قيمه Fr |
| $R = \frac{V \cdot y}{\nu}$ | $Fr = \frac{V}{\sqrt{g \cdot y}}$ |

| <u>Geometric similarity</u> | <u>Kinematic similarity</u> | <u>Dynamic similarity</u> |
|--|--|---|
| تعتمد هذه المجاملة على نقل للابعاد بنسبه واحدة | تعتمد هذه المجاملة على نقل السرعة وتعرف بنفس النسب | تعتمد هذه المجاملة على نقل القوى بنسبه |
| $L_r = \frac{L_m}{L_p}$ | $V_r = \frac{V_m}{V_p}$ | $F_r = \frac{F_m}{F_p}$ |

| <u>Permissible T.F</u> | <u>Critical T.F</u> |
|--|---|
| هو قيمه حوه اسحب داخل إقطاع والتي لا يحدث معها حركه حبيبات التراب مع اتجاه السريان | هو اقصى حوه سحب داخل المجرى لها قبل ان تبدأ بعض حبيبات التربه في حركه مع اتجاه السريان |

8

Dimensionally
homogenous

هي المعادلات التي يكون فيها ابعاد
الطرفين متساوية

non - Dimensionally
homogenous

هي المعادلات التي يكون فيها ابعاد
الطرفين غير متماثلة .

Hydraulically Smooth

عندما تكون الخشونة تكونه لقلع
القناة اقل من الخشونة الحرجه

$$K < K_c$$



Hydraulically Rough

عندما تكون ارتفاع خشونه داخل
المجرى المائي أكبر من الخشونة
الحرجه

$$K > K_c$$



Bed canal slopes:

$$S_o < S_c$$

(Mild slope)

$$S_o = S_c$$

(Critical slope)

$$S_o > S_c$$

(steep slope)

$$S_o = 0$$

(Horizontal)

$$S_o < 0$$

(Adverse slope)

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Define the Following Parameters :

1. Discharge rating curve,
2. Ultra rapid flow,
3. Types of open channels according to physical boundaries,
4. Best hydraulic section,
5. Dimensions of Chezy coefficient
6. Isovels,
7. Factors affect Manning coefficient,
8. $V_* = \text{-----} = \text{-----}$
9. Drag coeff.
10. Potential head,
11. Critical depth line,
12. For critical flow $y = \text{---}$, $IF = \text{---}$, $E = \text{---}$, $q = \text{---}$ and $F = \text{---}$,
13. For super-critical flow $y() Y_c$, $IF() 1.0$ and V is --- ,
14. for rectangular sec. $Y_c = \text{---}$, $V_c = \text{---}$ and $E_{min.} = \text{---}$,
15. Hydraulic jump,
16. Energy loss through jump,
17. efficiency of the jump,
18. Relative energy loss of the jump,
19. Advantages and disadvantages of modeling,
20. Types of similarity,
21. control section,
22. brink depth, and $Y_b = \text{---} Y_c$
23. Bed canal slopes,
24. Regimes of flow,
25. Sub-critical- Laminar flow,
26. Dimension analysis,
27. Roughness height,
28. Laminar sub-Layer,
29. Incipient motion,
30. Celerity,
31. Total energy line,
32. Dynamic equation of gradually varied flow and
33. Stagnation point.



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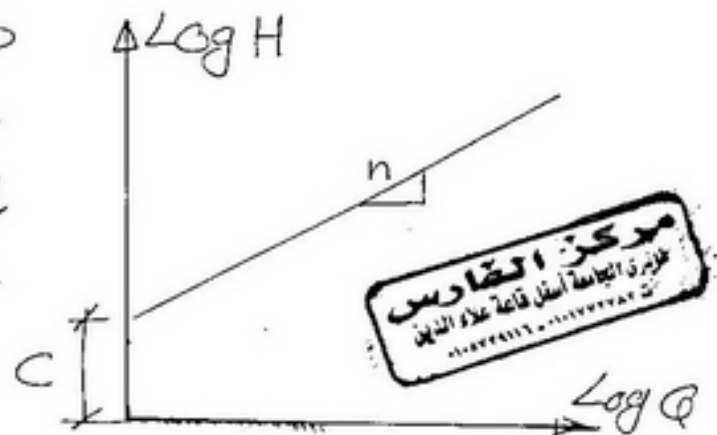


مركز الفارس للخدمات الطلابية
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مركز الفارس للخدمات الطلابية
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q = Discharge rating Curve

هو منحنى يتم اتقاؤه لعل
Current meter عبارة كجهاز
لمعرفة سرعة إريان بمعرفة
عدد لفات الجواز



Ultra rapid Flow: (Super critical flow)

هو إريان إذى تكون فيه قيمة $F > 1.0$

Types of Canals according to physical poundaries:

1 - natural Canals

قنوات طبيعية

2 - Artificial Canals

قنوات صناعية

Best Hydraulic section:

هو إقطاع إذى يعطى أخفى تصرف مع أقل حيط قبل عند
تبان المساحة .

Dimensions of Chezy Coeff.:

$$V = C \cdot \sqrt{R \cdot S}$$

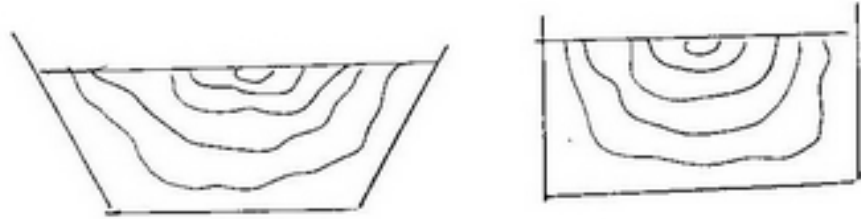
$$\therefore L \cdot T^{-1} = C \times \sqrt{\frac{L^2}{L} \times 1}$$

$$L \cdot T^{-1} = C \cdot L^{1/2} \Rightarrow$$

$$C = L^{1/2} \cdot T^{-1}$$

Isovels:

هذه مجموعة من الخطوط التخيلية التي تربط بينة لنقاط لها سرعة
في سره (داخل المقطاع العرضي للمجرى لهاي) .

Factors affecting Manning Coeff. (n):

- 1 - surface roughness. خشونة السطح
- 2 - Vegetation. وجود نباتات داخل المقطاع
- 3 - Canal irregularities. عدم انتظام المقطاع
- 4 - Canal alignment. تخطيط لقناة
- 5 - silting and scouring. الخروايز سيب داخل المجرى
- 6 - obstruction. وجود عوائق داخل المجرى لهاي

$$V_* = \sqrt{g \cdot R \cdot S} = \sqrt{\tau_0 / \rho}$$

Drag Coeff. :

هذه قوته قوى لقض المناقبة ضد السريان على الحدود
الصلبة للمقطع لهاي وتؤثر في نفس اتجاه حركته .

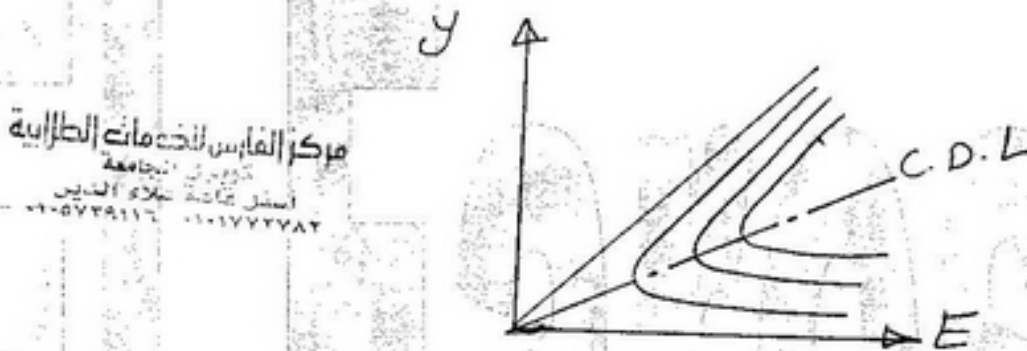
II potential head:

هو قيمة طاقة الوضع للسرطان مقارنة مع مستوى
قياسي (Z)

$$E = Z + y + \frac{V^2}{2g}$$

Critical depth line:

هو الخط المحدس الذي تقع عليه كل النقطة التي عرضها
نهر، لسيان هو النهر، يخرج وعليه قيمة 1.0



For critical Flow:

$$y = y_c, \quad F = 1.0, \quad E = E_{min} = 1.5 y_c$$
$$Q = Q_{max}, \quad F = F_{min} = 1.5 y_c^2$$

For super critical flow:

$$y < y_c, \quad F > 1, \quad V \text{ is max.}$$

For rectangular section:

$$y_c = \sqrt[3]{Q^2/g}, \quad E_{min} = 1.5 y_c$$

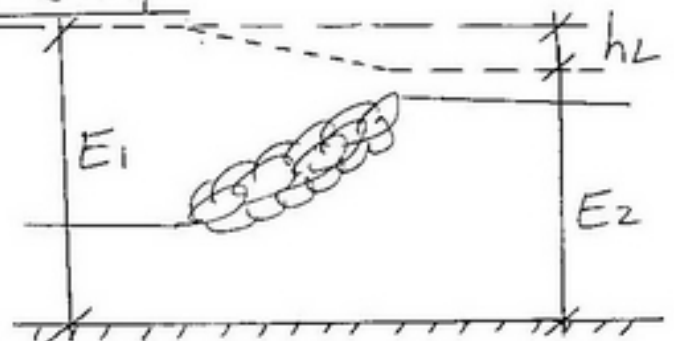
Hydraulic Jump:

هذه ظاهرة هيدروليكية تحدث نتيجة انتقال السريان من حالة sub critical الى حالة super critical

Energy loss through Jump:

$$h_L = E_1 - E_2$$

هذه مقدار الطاقة التي يتم تبديدها خلال القفزة



Efficiency of the Jump:

هذه قدره القفزة الهيدروليكية على نسبت الطاقة داخل

$$\eta = \frac{E_2}{E_1}$$

Relative energy loss of Jump:

هذه النسبة بين الطاقة البتتة داخل القفزة الهيدروليكية والطاقة الابتدائية للقفزة

$$\frac{h_L}{E_1}$$

Advantages of modeling

- ١- التوفير في التكاليف
- ٢- توفير في تكاليف البناء
- ٣- دراسة حالات تحليل معقدة

Disadvantage

- ١- عمل نماذج مكلف
- ٢- بعد القوى لتعليم تشغيل مملكتها
- ٣- (المرحوبه - الزلازل - ...)

13

Types of similarity:

- 1- geometric similarity.
- 2- Kinematic similarity.
- 3- Dynamic similarity.

Control section:

هو إقطاع الذي عليه تكونين العمق، لشرح للماء داخله،
و نستخدم في قياسه، لشرف.

* Brick depth $y_b = 0.7 y_c$

Regimes of Flow:



هو طريقة نستخدم لتصنيف
النواع السريان اعتماداً على
 F و R في نفس
الوقت

Sub critical Laminar Flow:

هو سريان الذي يكون فيه

$$F < 1$$

$$R < 500$$

14

Dimension analysis:

هذه طريقة تستخدم لربط المتغيرات المختلفة لوتره على
ظاهرة ما وإيجاد العلاقات بين هذه المتغيرات.

Roughness height:

هو مقدار ارتفاع الخشونة المكونة لجوانب وقاع الجاري
المائي.

Laminar sub layer:

هو طبقة من السريان بالقرب من قاع القناة وفيها
سيكون السريان مترامخ.

Incipient motion:

هو بداية حركه جسيمات التربة داخل القناة وتبدأ عندما
تصل فيه قوة السحب داخل الجري المائي إلى لفته الحرجه.

Celerity:

هو سرعه انتقال الموجه في المياه السطحية

$$V = \sqrt{g \cdot y}$$

Total energy Line:

هو خط يبين فيه الطاقة الكلية داخل الجري المائي
عند أي قطاع.



15

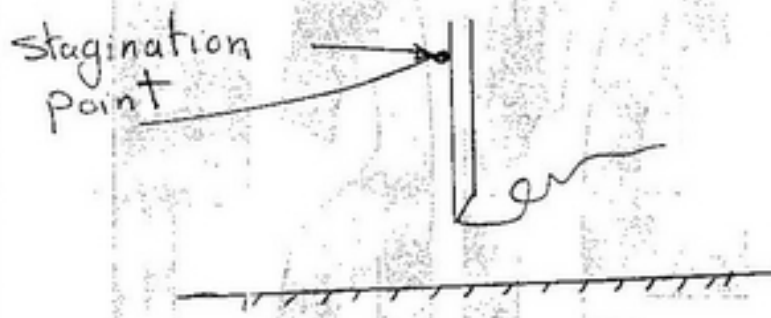
Dynamic equation of G.V.F.:

هذه المعادلة التي تستخدم لإيجاد العلاقة بين عمق المياه وتغيره مع المسافة الأفقية يمكن وضعها في عدة صور، منها

$$\frac{dy}{dx} = \frac{S_0 - S_e}{1 + \frac{V^2}{2g} \frac{d}{dy}}$$

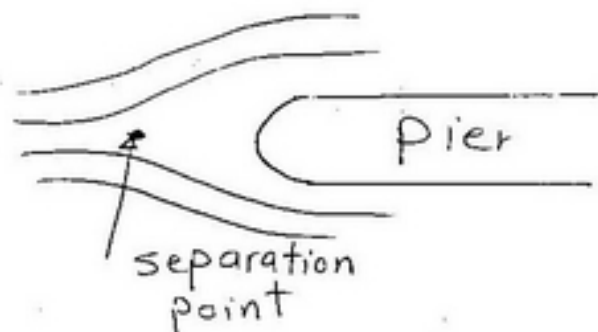
Stagnation point:

هذه النقطة التي تقل عندها سرعة السريان إلى الصفر وتحدث أمام البوابات



Separation point:

هذه النقطة التي يبدأ عندها انفصال خطوط السريان وتحدث أمام بقال التلباري.



16 velocity Head:

هو جزء من الطاقة ينتج من انتقال السريان بسرته
مقارنا (V) وقيمة $\left(\frac{V^2}{2g}\right)$

Relative initial depth:

هو النسبة بين العمق الابتدائي للقفزه، والعمق الحرجي
والطاقة عند بداية القفزه (y_1/E_1)

Dimension of Manning Coeff.:

$$\therefore V = \frac{1}{n} \cdot R^{2/3} \cdot S^{1/2}$$

$$L \cdot T^{-1} = \frac{1}{n} \cdot \left(\frac{L^2}{L}\right)^{2/3} \cdot 1$$

$$L \cdot T^{-1} = \frac{1}{n} \cdot L^{2/3}$$

$$\therefore n = \frac{L^{2/3}}{L \cdot T^{-1}}$$

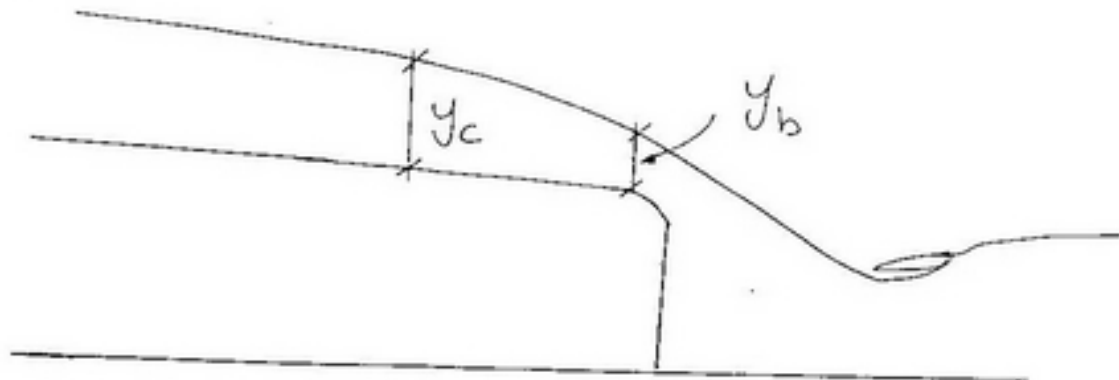
$$n = L^{-1/3} \cdot T$$

Current meter:

هو جهاز يستخدم لتحديد سرته بناء داخل القنوات
المائية.

17

How a brink measure the discharge:



$$\therefore y_c = 0.7 y_b$$

بجانب y_b على الماء y_c

$$\therefore y_c^3 = q^2 / g$$

بجانب q على الماء y_c

$$Q = q \times B$$

Defferent Models

Compare Between Each Of :

1. Effect of vegetation and roughness on Manning Coeff.,
2. Effect of curvature with large and small radius on Manning Coeff.,
3. Chute and drops,
4. Shallow wide sec. and narrow deep sec,
5. Efficient sec. and economic sec,
6. Rapidly varied flow and gradually varied flow,
7. IR_* and IR ,
8. A , R , Y , Y_1 and Z ,
9. Specific energy and total energy,
10. Alternative depths and conjugate depths,

Define the Following Parameters :

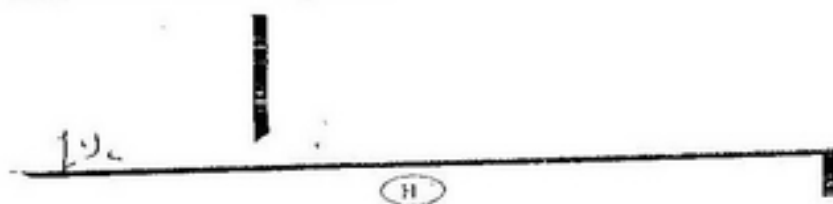
1. Discharge rating curve,
2. Ultra rapid flow,
3. Types of open channels according to physical boundaries,
4. Best hydraulic section,
5. Dimensions of Manning coefficient,
6. Isovels,
7. Factors affect Manning coefficient,
8. $V_* = \frac{V}{\sqrt{gD}} = \frac{V}{\sqrt{gR}} = \frac{V}{\sqrt{gY}}$
9. Drag coeff.
10. Potential head,

Give Neat Sketch For Each Case :

1. The relationship between Y_1 and Y_2 and Z ,



2. The water surface profile



Compare Between Each Of:

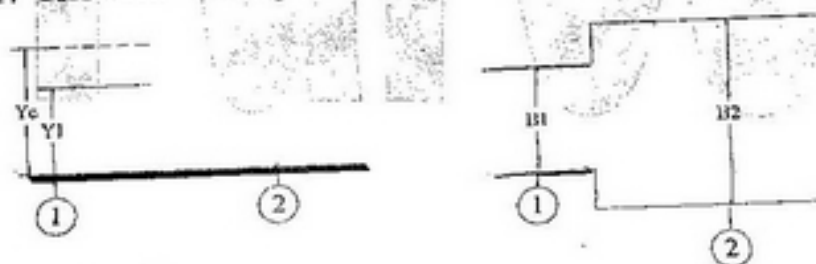
1. Chute and drops,
2. Shallow wide sec. and narrow deep sec,
3. Efficient sec. and economic sec,
4. IR. and IR,
5. Actual shear stress and critical shear stress,
6. Specific energy, discharge and force diagrams,
7. Ideal and Elastic fluids,
8. Open channel flow and Pipe flow,
9. Effect of viscosity and effect of gravity on the flow,
10. Geometric, kinematics and dynamic similarity,

Define the Following Parameters :

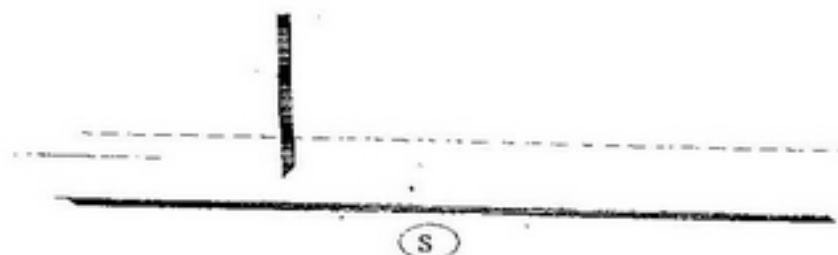
11. Regimes of flow,
12. Sub-critical- Laminar flow,
13. Dimension analysis,
14. Roughness height,
15. Laminar sub-Layer,
16. How a brink can be measure the discharge,
17. Celerity,
18. Total energy line,
19. Dynamic equation of gradually varied flow and
20. Stagnation point.

Give Neat Sketch For Each Case :

1. The relationship between Y_1 and Y_2 and B_2 ,



2. The water surface profile



Compare Between Each Of:

1. Normal velocity and shear velocity,
2. IR_* and IR ,
3. Actual shear stress and critical shear stress,
4. Specific energy and total energy,
5. Velocity correction factor and momentum correction factor,
6. Alternative depths and conjugate depths,
7. Critical, sub-critical and super-critical flow,
8. Ideal and Elastic fluids,
9. Newtonian and Non-Newtonian fluids,
10. Open channel flow and Pipe flow,

Define the Following Parameters :

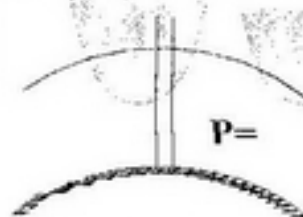
1. For critical flow $y = --$, $IF = --$, $E = --$, $q = --$ and $F = --$,
2. Energy loss through jump,
3. Relative initial depth of the jump,
4. Types of similarity,
5. control section,
6. brink depth, and $Y_b = ---- Y_c$
7. Bed canal slopes,
8. Current meter,
9. Regimes of flow,
10. Sub-critical- Laminar flow,

Give Neat Sketch For Each Case :

- 1- The pressure inside the pizometer for each case,

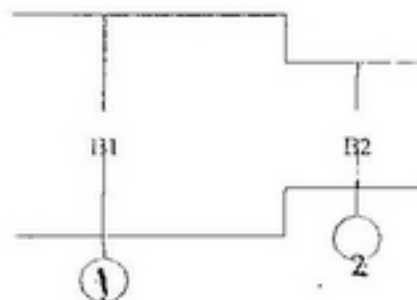
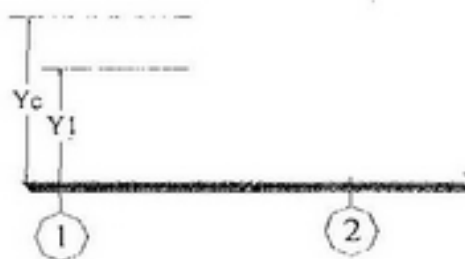


Convex



Concave

3. The relationship between Y_1 and Y_2 and B_2 ,



Compare Between Each Of:

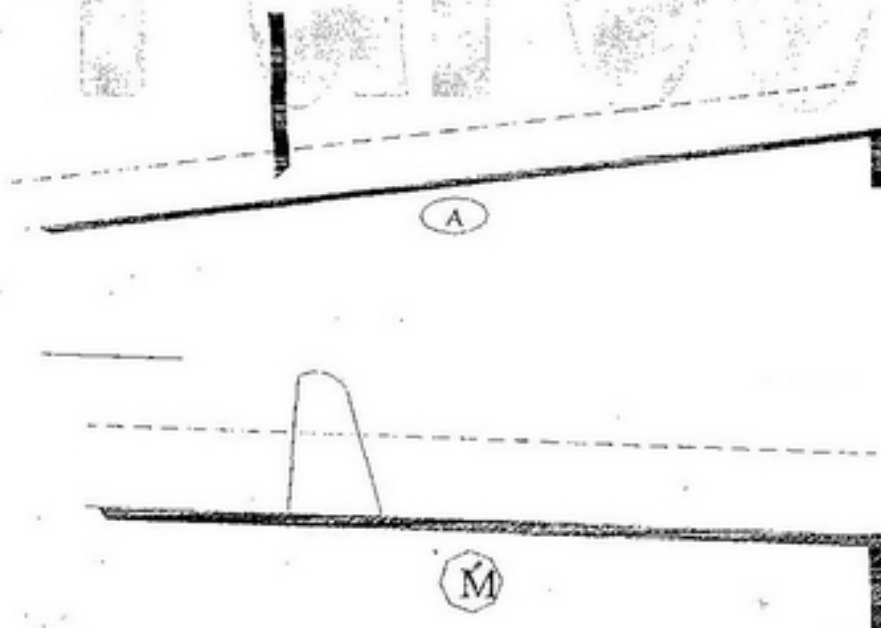
1. Manning and Chezy Eqs.,
2. Canal and flume,
3. Efficient sec. and economic sec,
4. Normal velocity and shear velocity,
5. Specific energy and total energy,
6. Specific energy, discharge and force diagrams,
7. Newtonian and Non-Newtonian fluids,
8. Effect of viscosity and effect of gravity on the flow,
9. Dimensionally and non- dimensionally homogeneous,
10. Hydraulically smooth and Hydraulically rough surface and

Define the Following Parameters :

1. Discharge rating curve,
2. Best hydraulic section,
3. Dimensions of Manning coefficient,
4. Drag coeff.
5. Potential head,
6. critical depth line,
7. For critical flow $y = \dots$, $IF = \dots$, $E = \dots$, $q = \dots$ and $F = \dots$,
8. for rectangular sec. $Y_c = \dots$, $V_c = \dots$ and $E_{min} = \dots$,
9. Relative energy loss of the jump,
10. Advantages and disadvantages of modeling,

Give Neat Sketch For Each Case :

4. The water surface profile



Compare Between Each Of :

- ✓ 1. Chute and drops,
- ✓ 2. Shallow wide sec. and narrow deep sec,
- ✓ 3. Laminar and turbulent flow,
- ✓ 4. Rapidly varied flow and gradually varied flow,
- ✓ 5. Actual shear stress and critical shear stress,
- ✓ 6. Velocity correction factor and momentum correction factor,
- ✓ 7. Alternative depths and conjugate depths,
- ✓ 8. Specific energy, discharge and force diagrams,
- ✓ 9. Critical, sub-critical and super-critical flow,
- ✓ 10. Ideal and Elastic fluids,

Define the Following Parameters :

- ✓ 1. Ultra rapid flow,
- ✓ 2. Types of open channels according to physical boundaries,
- ✓ 3. Isovels,
- ✓ 4. Factors affect Manning coefficient,
- ✓ 5. Velocity head,
- ✓ 6. For super-critical flow $y(<)Y_c$, IF $(>)1.0$ and V is ----,
- ✓ 7. Hydraulic jump,
- ✓ 8. Jump height,
- ✓ 9. efficiency of the jump,
- ✓ 10. Relative initial depth of the jump,

Give Neat Sketch For Each Case :

1. The water surface profile



Compare Between Each Of:

1. Effect of vegetation and roughness on Manning Coeff.,
2. Canal and flume,
3. Shallow wide sec. and narrow deep sec.,
4. Laminar and turbulent flow,
5. Average normal velocity and shear velocity,
6. Actual shear stress and critical shear stress,
7. Specific energy and total energy,
8. Alternative depths and conjugate depths,
9. Ideal and Elastic fluids,
10. Stream line, Streak line, Path line and stream tube,

Define the Following Parameters :

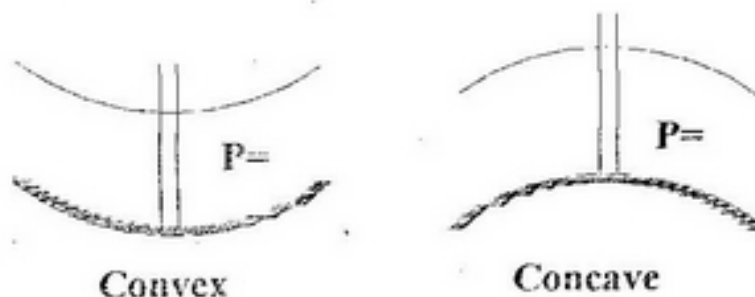
1. Types of open channels according to physical boundaries,
2. Dimensions of Chezy coefficient
3. Isovels,
4. Critical depth line,
5. For critical flow $y = \dots$, $IF = \dots$, $E = \dots$, $q = \dots$ and $F = \dots$,
6. For super-critical flow $y() Y_c$, $IF() 1.0$ and V is \dots ,
7. for rectangular sec. $Y_c = \dots$, $V_c = \dots$ and $E_{min} = \dots$,
8. brink depth, and $Y_b = \dots Y_c$
9. Bed canal slopes,
10. Regimes of flow,

Give Neat Sketch For Each Case :

1. The water surface profile

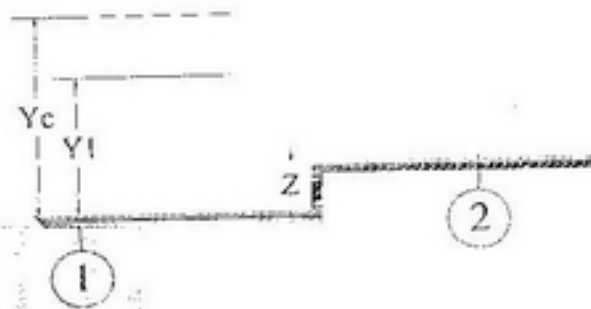


2. The pressure inside the pizometer for each case,

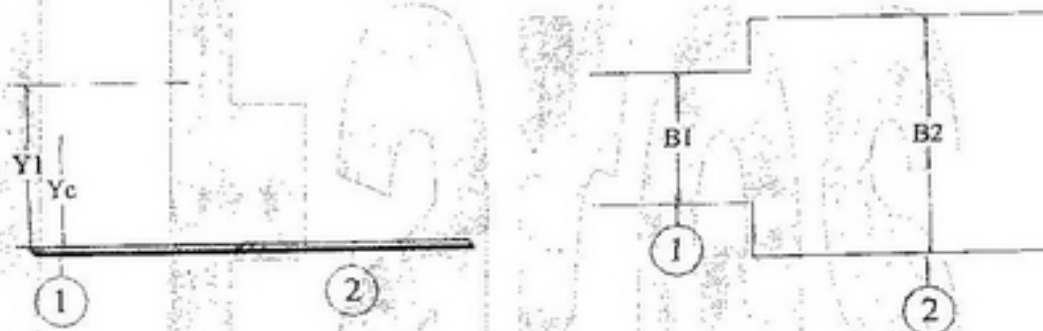


Give Neat Sketch For Each Case :

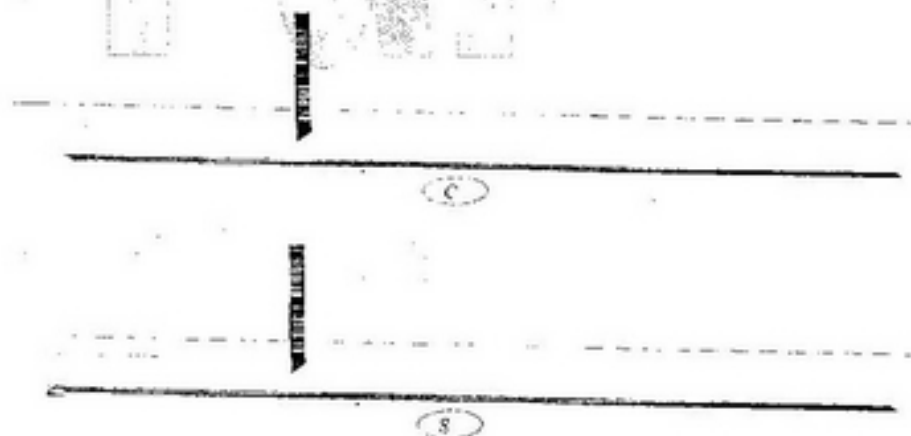
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8. Open channel flow and Pipe flow,
9. Geometric, kinematics and dynamic similarity,
10. Permissible and critical tractive forces,
11. Dimensionally and non- dimensionally homogeneous,
12. Hydraulically smooth and Hydraulically rough surface and
13. the bed canal slopes.

Define the Following Parameters :

1. Discharge rating curve,
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6. Isovels,
7. Factors affect Manning coefficient,
8. $V_* = \frac{V^2}{\nu} = \frac{\tau_0}{\rho \nu}$
9. Drag coeff.
10. Potential head,
11. Critical depth line,
12. For critical flow $y = y_c$, $IF = 1$, $E = 1.5$, $q = 1.486 K^{1/2} S^{1/2} y_c^{3/2}$ and $F = 1$,
13. For super-critical flow $y < y_c$, $IF < 1$ and V is $> V_c$,
14. for rectangular sec. $Y_c = \frac{V^2}{g}$, $V_c = \frac{g Y_c}{V}$ and $E_{min} = 1.5$,
15. Hydraulic jump,
16. Energy loss through jump,
17. efficiency of the jump,
18. Relative energy loss of the jump,
19. Advantages and disadvantages of modeling,
20. Types of similarity,

Fin

MCQ on Open-Channel Flow

1. Open-channel flows have a pressure force driving the fluid similar to pipe flows. True or False

☐ A. True

☒ B. False

2. Where did the greatest difference between high and low tide occur?

☒ A. The Bay of Fundy, Canada

☐ B. Lundy's Lane, Canada

☐ C. The coast of Maine, U.S.A.

3. Open channel flow can have more than one characteristic. True or False

☒ A. True

☐ B. False

4. The surface of a lake or ocean is often distorted into changing patterns associated with ____.

☐ A. Evaporation

☐ B. Uniform flow

☒ C. Surface waves

5 missing

6. The speed of a small amplitude, solitary wave is proportional to the ____ of the fluid depth.

Answer:

square root

7. The wave speed can be obtained from the continuity and energy equations. True or False

☐ A. True

☒ B. False

8. What does the term c represent in wave equations?

☐ A. Wave depth

☒ B. Wave speed

☐ C. Amplitude

9. How is wave speed measured?

☒ A. Relative to the flow

☐ B. Relative to a fix position on the ground

☐ C. Relative to the acceleration of the wave

10. What assumption is made about the slope of the channel bottom in most open channel flows?

☐ A. The surface is rough.

☒ B. The slope is assumed to be constant.

☐ C. The slope is assumed to be negative

1. According to the specific energy diagram, how many possible depths, with some physical meaning, are there for given flow rate and specific energy, assuming $E > E_{min}$?

☐ A. One

☒ B. Two

☐ C. Three

The rate of change of the fluid depth depends on the local ____ of the channel bottom, the ____ of the energy line, and the Froude number.

Answer:

Slope, slope

13. How is uniform depth flow achieved?

- ☒ A. By adjusting the bottom slope to equal the slope of the energy line.
- ☐ B. By adjusting the flow speed so that it equals the energy line
- ☐ C. By ensuring uniform laminar flow

14. The wetted perimeter includes the free surface for open-channel flows. True or False

- ☐ A. True
- ☒ B. False

15. Where does the wall shear stress act in open-channel flow?

- ☐ A. Along the entirety of the flow.
- ☒ B. On the wetted perimeter.
- ☐ C. Only on the free surface

16. The velocity profile in an open channel is uniform. True or False

- ☐ A. True
- ☒ B. False

17. Are most open-channel flows laminar or turbulent?

Answer: Turbulent

18. The Manning equation is used to obtain the ____ or flow rate in an open channel.

- ☐ A. Flow rate
- ☐ B. Density
- ☒ C. Velocity

19. The value of the Manning coefficient, n , depends on what?

- ☒ A. The nature of the channel surface
- ☐ B. The mass flow rate of the flow
- ☐ C. The type of fluid

20. What shape provides the best hydraulic cross section for open-channel flows?

- ☐ A. A circular pipe
- ☒ B. A semicircular channel
- ☐ C. A triangular channel

21. What three classifications are open-channel flows divided into?

Answer:

uniform depth, gradually varying
rapidly varying

22. How many different surface shape designations are there for free surface calculations?

Answer:

12

23. On what two factors does the free surface shape depend on?

Answer:

The channel bottom slope and
The Froude number

24. What is the technical term for a discontinuity in the free surface elevation of channel flow?

- ☒ A. A hydraulic jump
- ☐ B. A rectangular channel
- ☐ C. Rapidly varied flow

25. What is the primary cause of the head loss that occurs across a hydraulic jump?

- ☐ A. An increase in flow depth

- ☒ B. Turbulent mixing
☐ C. A change in momentum

26. What function of the upstream flow dictates the depth ratio across a hydraulic jump?

- ☐ A. The mass flow rate
☒ B. The velocity of the flow
☐ C. The Froude number

27. The length of a hydraulic jump can be determined analytically. True or False

- ☒ A. True
☐ B. False

28. What are the two main mechanisms governing the flow over a weir?

Answer:

Inertia and gravity

29. What happens to the velocity of the flow as it passes over a broad-crested weir?

- ☐ A. It decelerates
☒ B. Nothing
☐ C. The flow accelerates and reaches critical condition.

MCQ on Dimensional Analysis, Similitude, and Modeling

1. The pressure drop per unit length that develops due to friction cannot generally be solved analytically.

☒ A. True
☐ B. False

2. A qualitative description of physical quantities can be given in terms of ____.

Answer:

BASIC DIMENSION

3. Dimensional analysis is the when the results of an equation will be what in relation to the system of units chosen.

☒ A. Dependent
☒ B. Independent
☐ C. Constant

4. Dimensional analysis is based on the ____.

Answer:

Buckingham pi theorem

5. The dimensions of the variable on the left side of the equation must be ____ the dimensions of any term that stands by itself on the right side of the equal sign.

☒ A. Greater than
☒ B. Equal to
☐ C. Fewer than

6. The required number of pi terms is what compared to the number of original variables?

☐ A. Greater than

- ☐ B. Equal to
- ☒ C. Fewer than

7. The most difficult step in the method of repeating variables is ____.

- ☒ A. Listing all of the variables that are involved in the problem
- ☐ B. Express each of the variables in terms of basic dimensions
- ☐ C. Determine the required number of pi terms

8. The number of variables is desired to be kept to a minimum so that the amount of ____ can be kept to a minimum.

Answer:

Laboratory work

9. When using the repeating variables method, the number of repeating variables that are selected should be what compared to the number of reference dimensions?

- ☐ A. Greater than
- ☒ B. Equal to
- ☐ C. Less than

10. The pi terms must always be what?

- ☐ A. Negative
- ☐ B. Equal in dimensions
- ☒ C. Dimensionless

11. How many steps are there in the method of repeating variables?

Answer:

8

12. If too many pi terms appear in the final solution then the problem may be difficult, time consuming, and ____ to eliminate these experimentally.

Answer: _____

EXPENSIVE

13. Variables can be classified into three general groups: geometry, material properties, and external effects.

☒ A. True

☐ B. False

14. An external effect is used to denote any variable that produces or tends to produce what?

☐ A. Inaccurate results

☐ B. Constant results

☒ C. Change in the system

15. How many different points are there to consider in the selection of variables?

☐ A. 3

☒ B. 6

☐ C. 8

16. Typically, in fluid mechanics the required number of reference dimensions is ____.

Answer: _____

Three

17. Where does any other set of pi terms besides the original set come from?

Answer: _____

Mam pulation of a corrected set of terms

18. The number of required pi terms is fixed in accordance with the pi theorem.

- ☒ A. True
☐ B. False

19. How many restrictions are there for pi terms?

- ☐ A. None
☒ B. Two
☐ C. Three

20. Pi terms can be formed by inspection by simply making use of the fact that each pi term must be dimensionless.

- ☒ A. True
☐ B. False

21. Which of the following is equivalent to the repeating variable method?

- ☒ A. Forming pi terms by inspection
☐ B. Forming pi terms by dimensional analysis
☐ C. Determination of reference dimensions

22. A useful physical interpretation can often be given to dimensionless groups.

- ☒ A. True
☐ B. False

23. Write the Reynolds number equation.

Answer:

$$Re = \frac{\rho V L}{\mu}$$

24. What is the symbol for the Cauchy number?

- ☐ A. Cn

- ☒ B. Ca
☐ C. Cu #

25. The Weber number is a relationship between the inertial force and what other force?

- ☒ A. Surface tension
☐ B. Kinetic
☐ C. Frictional

26. Flows with very small Reynolds numbers are commonly referred to as "_____".

Answer:

Creeping flows

27. The Euler number is undoubtedly the most famous dimensionless parameter in fluid mechanics.

- ☐ A. True
☒ B. False

28. The Mach number and what other number cannot be used in the same problem?

- ☐ A. Euler number
☐ B. Reynolds number
☒ C. Cauchy number

29. The flow of river water is significantly affected by surface tension.

- ☐ A. True
☒ B. False

30. The fewer the number of pi terms the more simple the problem.

- ☒ A. True

☐ B. False

31. For problems involving only two pi terms, results of an experiment can be conveniently presented in _____.

Answer:

A simple graph

32. For complicated problems it is often less feasible to use models to predict specific characteristics of the system than to develop general correlations.

☐ A. True

☒ B. False

33. A representation of a physical system that may be used to predict the behavior of the system in some desired respect is what?

☐ A. Prototype

☒ B. Model

☐ C. Facsimile

34. Model design conditions are also called similarity requirements or modeling laws.

☒ A. True

☐ B. False

35. The second similarity requirement indicates that the model and the prototype must be operated at _____.

Answer:

The same Reynolds' number

36. When velocity ratios and acceleration ratios are constant throughout the flow field, kinematic similarity exists between the model and the prototype.

☒ A. True

☐ B. False

37. For true models, how many scales will there be?

☐ A. None

☒ B. One

☐ C. As many as needed

38. Models for which one or more of the similarity requirements are not satisfied are called _____ models.

Answer:

Distorted

39. Distorted models cannot be successfully used, only true models can be accurately used.

☐ A. True

☒ B. False

40. Geometric and Reynolds number similarity is usually not required for models involving flow through closed conduits.

☐ A. True

☒ B. False

41. For large Reynolds numbers, the inertial forces are _____ the viscous forces?

☐ A. Less than

☐ B. Approximately the same as

☒ C. Larger than

42. For a Length Scale of 1/10 and a prototype velocity of 30 mph, what is the required model velocity?

Answer:

300 mph

43. How do the dimples on a golf ball effect drag?

- ☒ A. they reduce drag
- ☐ B. they increase drag
- ☐ C. they do not effect drag

44. When the Mach number becomes greater than approximately ____, the influence of compressibility becomes significant.

Answer:

0.3

45. Flows in canals, rivers, spillways, and stilling basins are all examples of flows with a free surface.

- ☒ A. True
- ☐ B. False

46. At temperatures of -20°F , what is the ice growth rate that can be achieved.

- ☐ A. 1-mm per hour
- ☒ B. 2-mm per hour
- ☐ C. 3-mm per hour

47. The drag on a ship depends on both the Reynolds number and the Froude number.

- ☐ A. True
- ☒ B. False

48. Similarity laws can be directly developed from the ____ governing the phenomenon of interest.

Answer:

Equation

49. For time-dependant problems, which of the following is crucial for successfully finding a solution?
- ☐ A. The derivative of the equation
 - ☒ B. Initial conditions
 - ☐ C. The velocities at all points
50. Governing equations expressed in terms of dimensionless variables lead to the appropriate dimensionless groups.
- ☒ A. True
 - ☐ B. False
51. The Froude number arises because of the inclusion of what in a problem?
- ☐ A. Pressure
 - ☐ B. Velocity
 - ☒ C. Gravity
52. From this section it can be concluded that for the steady flow of a compressible fluid without free surfaces, dynamic and kinematic similarity will be achieved.
- ☐ A. True
 - ☒ B. False

Final Exam of Hydraulics 2009

Question (1)

A)

| Hydraulically smooth | Hydraulically roughness |
|---|---|
| <p>1- Roughness don't effecting on velocity distribution</p> <p>2- $K < \delta_0$</p> $\frac{u_* \cdot k}{\nu} < 5$ $U = 2.5U_* \ln \frac{9yU_*}{\nu}$ | <p>1- Roughness effecting on velocity distribution</p> <p>2- $K > \delta_0$</p> $\frac{u_* \cdot k}{\nu} > 5$ $U = 2.5U_* \ln \frac{30y}{k}$ |
| Best hydraulic section | Stable section |
| <p>- Its section is passing maximum discharge for minimum wetted perimeter at constant manning coefficient, water area and longitudinal slope.</p> | <p>-Its section not permissible to scouring or silting.</p> |
| Friction velocity(shear velocity) | Mean flow velocity |
| <p>Its maximum velocity in channel before the particle of side and bed to move.</p> $U_* = \sqrt{gRS}$ | <p>$Q = A \cdot V$ Q=discharge m³/s A water area V Mean flow velocity m/s</p> |
| State of flow | Regime of flow |
| <p>When we study behavior of flow according to</p> <p>1-effect of viscosity</p> $IR = \frac{V \cdot R}{\nu}$ <p>$IR \leq 500$ flow is laminar $500 < IR \leq 2000$ flow is transitional $IR > 2000$ flow is turbulent</p> <p>1-effect of gravity</p> $FI = \frac{V}{\sqrt{g \cdot y_h}}$ <p>$FI < 1$ flow is sub critical $FI = 1$ flow is critical $FI > 1$ flow is super critical</p> | <p>When we take effect of gravity and viscosity the flow classified in the following cases</p> <p>1- $IR < 500$ & $FI < 1$ flow is laminar-sub critical 2- $IR < 500$ & $FI > 1$ flow is laminar-superb critical 3- $IR > 2000$ & $FI < 1$ flow is turbulent-sub critical 4- $IR > 2000$ & $FI > 1$ flow is turbulent-super critical</p> |

Given

A.S = 65,000 fed & W.D = 56 m³/fed/day
S = 10 cm/km & Z = 1.00
n = 0.025
Trapezoidal section

Req

Design of sec for the following cases

- 1- $V_{\max} = 0.58$ m/s
- 2- ζ (max shear stress) = 0.22 kg/m²

Solutions

a) For maximum velocity

$$Q = \frac{A.S * W.D}{24 * 60 * 60} = \frac{65,000 * 56}{24 * 60 * 60} = 42.13 \dots m^3/sec$$

$$Q = A * V \dots A = \frac{Q}{V} = \frac{42.13}{0.58} = 72.64 \dots m^2$$

$$A = y(b + zy) = 72.64 \dots y(b + 1 * y) = 72.64 \dots 1$$

—By using manning equation

$$Q = \frac{1}{n} * \frac{A^{5/3}}{P^{2/3}} * S^{1/2} \dots m^3/sec \dots 42.13 = \frac{1}{0.025} * \frac{(72.64)^{5/3}}{(b + 2y\sqrt{1+z^2})^{2/3}} * (10 * 10^{-5})^{1/2}$$

$$b + 2y\sqrt{1+(1)^2} = 41.605 \dots b = 41.605 - 2.83y \dots 2 \quad \text{Sub in}$$

1

$$72.64 = y(41.605 - 2.83y + y) \dots 72.64 = 41.605y - 1.83y^2$$

$$y^2 - 22.73y + 39.694 = 0.00$$

$$\text{Get } y = 1.906 \text{ m} \quad \& \quad b = 36.21 \text{ m}$$

b) For maximum shear stresses

$$\zeta \text{ (max shear stress)} = 0.22 \text{ kg/m}^2$$

$$\zeta = \gamma * R * S$$

$$0.22 = 1000 * R * 10 * 10^{-5} \dots R = 2.2 \text{ m}$$

$$V = \frac{1}{n} * R^{2/3} * S^{1/2} \dots m^3/sec \dots V = \frac{1}{0.025} * (2.2)^{2/3} * (10 * 10^{-5})^{1/2}$$

$$\underline{V=0.667\text{m/s}}$$

$$Q = A \cdot V \dots\dots\dots A = \frac{Q}{V} = \frac{42.13}{0.667} = 62.23 \dots \text{m}^2$$

----By using manning equation

$$Q = \frac{1}{n} \cdot \frac{A^{5/3}}{P^{2/3}} \cdot S^{1/2} \dots \text{m}^3/\text{sec} \dots\dots\dots 42.13 = \frac{1}{0.025} \cdot \frac{(62.23)^{5/3}}{(b + 2y\sqrt{1+z^2})^{2/3}} \cdot (10 \cdot 10^{-3})^{1/2}$$

$$b + 2y\sqrt{1+(1)^2} = 28.38 \dots\dots\dots b = 28.38 - 2.83y \dots\dots\dots 2 \text{ Sub in 1}$$

$$62.27 = y(28.38 - 2.83y + y) \dots\dots\dots 62.274 = 28.385y - 1.83y^2$$

$$y^2 - 15.44y + 34.03 = 0.00$$

$$\underline{\text{Get } y=2.663 \text{ m} \quad \& \quad b=20.84\text{m}}$$

-To compare excavation cost

1-By using max velocity

$$A = 72.64 \dots \text{m}^2$$

2-By using max shear stress

$$A = 62.23 \dots \text{m}^2$$

The cost of excavation in design by max excavation more than design by max shear stress

-To show regime of flow

1-By using max velocity

$$y_h = \frac{A}{T} = \frac{72.64}{(36.21 + 2 \cdot 1.000 \cdot 1.9063)} = \frac{42.64}{40.0226} = 1.0654\text{m} -$$

$$FI = \frac{V}{\sqrt{g \cdot y_h}} = \frac{[0.58]}{[\sqrt{9.81 \cdot 1.0654}]} = 0.179 < 1.00 \dots\dots\dots \text{sub} \dots \text{critical} \dots \text{flow}$$

$$R = \frac{A}{P} = \frac{72.64}{[36.21 + 2 \cdot 1.906 \sqrt{1 + (1.00)^2}]} = \frac{68.6133}{41.6018} = 1.649$$

$$IR = \frac{V \cdot R}{\nu} = \frac{(0.58) \cdot (1.649)}{1 \cdot 10^{-6}} = 956,586.35 > 2000 \dots\dots\dots \text{turbulent} \dots \text{flow}$$

Flow is sub critical turbulent

1-By using max shear stress

$$y_h = \frac{A}{T} = \frac{62.23}{(20.84 + 2 * 1.000 * 2.663)} = \frac{42.64}{26.166} = 1.63m -$$

$$Fr = \frac{V}{\sqrt{g * y_h}} = \frac{[0.667]}{[\sqrt{9.81 * 1.63}]} = 0.167 < 1.00 \dots \text{sub} \dots \text{critical} \dots \text{flow}$$

$$R = \frac{A}{P} = \frac{72.64}{[20.84 + 2 * 2.663 \sqrt{1 + (1.00)^2}]} = \frac{68.6133}{28.372} = 2.418$$

$$IR = \frac{V * R}{\nu} = \frac{(0.667) * (2.418)}{1 * 10^{-6}} = 1,612,806 > 2000 \dots \text{turbulent} \dots \text{flow}$$

Flow is sub critical turbulent

Question (2)

A)

-specific energy

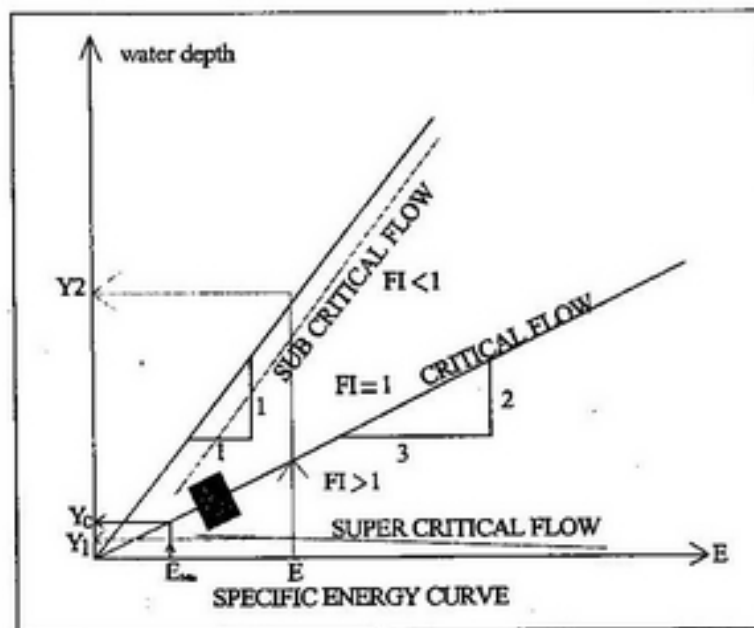
$$E = y + \frac{V^2}{2g} = y_2 + \frac{Q^2}{2 * g * A^2}$$

-total specific energy

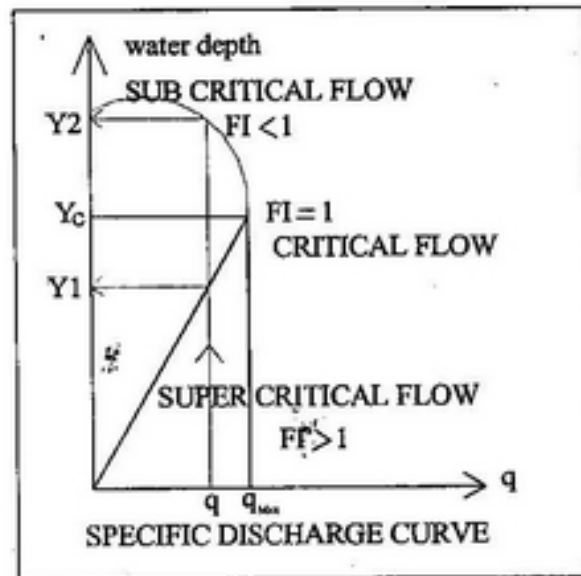
$$E = Z + y + \frac{V^2}{2g} = Z + y_2 + \frac{Q^2}{2 * g * A^2}$$

-two alternative depth

Its two depths have the same specific energy and discharge one of them more than critical depth and occur in sub critical flow and other less than critical depth and occur in super critical flow



Specific energy diagram show relation between (E - Y) this curve draw under line slope 1: 1 (angle of 45°) .there are another line draw by slope 3: 2 (critical depth line) at y_c occurs minimum specific energy ($y_c = 1.50 E_{min}$). If y less than y_c flow is super critical and If y more than y_c flow is sub critical.



Specific discharge diagram show relation between ($q - Y$) and at y_c occurs maximum specific discharge, if y less than y_c flow is super critical and if y more than y_c flows is sub critical.

B)

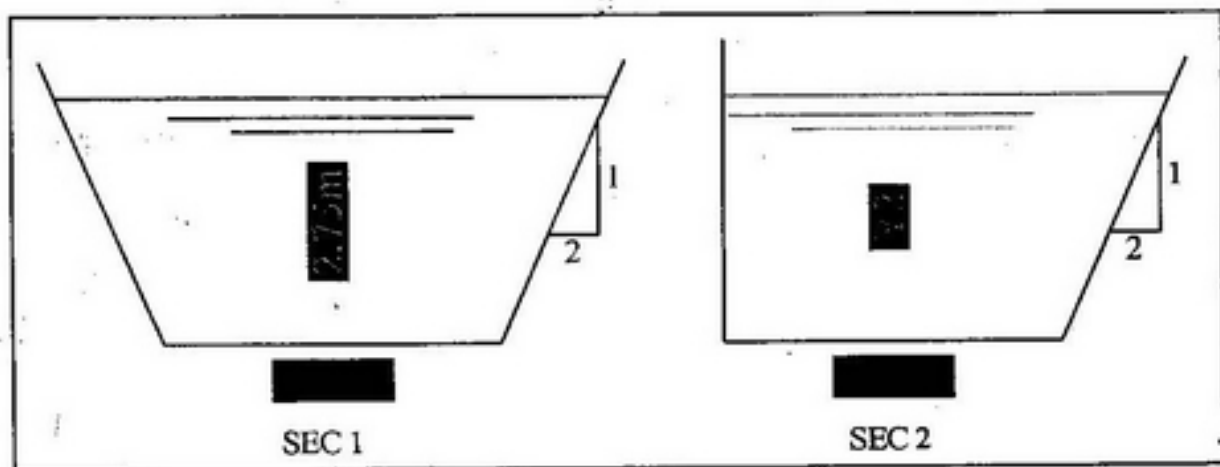
Given

$Q=23\text{m/s}$ & $z=2$
 $b=8.00\text{m}$ & $y=2.75\text{m}$
Trapezoidal section

Required

1-water depth at contraction
2-max height of hump

Solution



1) To get water depth

Applying energy equation between section 1 and section 2

$$E_1 = E_2 + h_L$$

By neglecting head loss

$$E_1 = E_2$$

$$A = y(b + zy) = 2.75(8 + 2 \cdot 2.75) = 37.125 \dots m$$

$$y_1 + \frac{Q^2}{2g \cdot A_1^2} = y_2 + \frac{Q^2}{2g \cdot A_2^2}$$

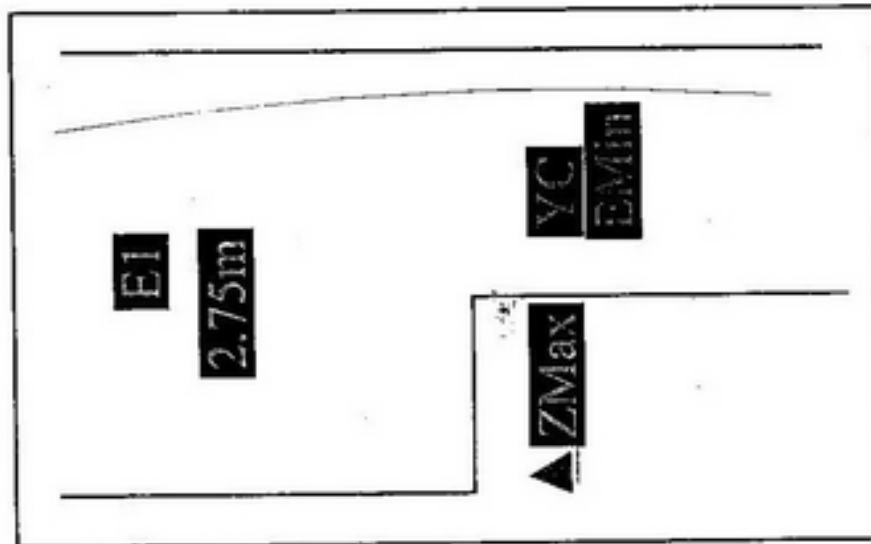
$$2.75 + \frac{(23)^2}{2 \cdot 9.81 \cdot 37.125^2} = y_2 + \frac{23.00^2}{2 \cdot 9.81 \cdot (6y_2 + y_2^2)^2}$$

$$2.7696 = y_2 + \frac{26.962}{(6y_2 + y_2^2)^2}$$

By trial and error

$$Y_2 = 2.72m$$

2- To get ΔZ_{max}



$$E_1 = E_{min} + \Delta Z_{max}$$

$$y_1 + \frac{Q^2}{2g \cdot A^3} = E_{min} + \Delta Z_{max}$$

$$E_{min} = y_c + \frac{y_h}{2}$$

$$\frac{Q^2}{g} = \frac{A^3}{T} \quad \frac{(23.00)^2}{9.81} = \frac{(6y_c + y_c^2)^3}{(6 + 2y_c)} \quad 53.925 = \frac{(6y_c + y_c^2)^3}{(6 + 2y_c)}$$

By trial and error

$$Y_c = 1.075m$$

$$y_h = \frac{A}{T} = \frac{(b \cdot y_c + y_c^2)}{(b + 2 \cdot y_c)} \quad y_h = \frac{(6 \cdot 1.075 + (1.075)^2)}{(6 + 2 \cdot 1.075)} = 0.9332$$

$$E_{min} = y_c + \frac{y_h}{2} = 1.075 + \frac{0.9332}{2} = 1.5416m$$

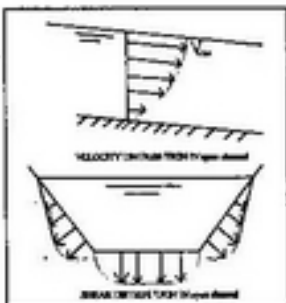
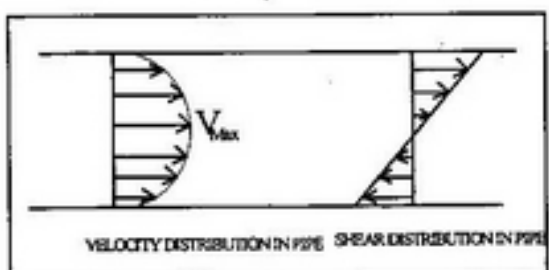
$$E_{min} = y_c + \frac{y_c(2.50 + 1.50y_c)}{2(2.50 + 2 \cdot 1.50 \cdot y_c)} = 2.00$$

$$y_1 + \frac{Q^2}{2g \cdot A^3} = E_{min} + \Delta Z_{max} \quad 2.75 + \frac{(23)^2}{2 \cdot 9.81 \cdot 37.125^2} = 1.5416 + \Delta Z_{max}$$

$$\Delta Z_{max} = 1.2m$$

QUESTION (3)

A)

| Open channel | pipe |
|---|---|
| <p>1-main force affecting on flow is inertia force and gravity force.</p> <p>2-main dimensionless number described low is Froude number</p> <p>3-natural or artificial</p> <p>4-for $IR \leq 500$ flow is laminar $500 < IR \leq 2000$ flow is transitional $IR > 2000$ flow is turbulent</p> <p>5- Velocity distribution shear distribution</p> | <p>1-main force affecting on flow is inertia force and viscosity force.</p> <p>2-main dimensionless number described flow is Renold number</p> <p>3- artificial</p> <p>4-for $IR \leq 200$ flow is laminar $2000 < IR \leq 4000$ flow is transitional $IR > 4000$ flow is turbulent</p> <p>5- Velocity distribution shear distribution</p> |
|  <p>VELOCITY DISTRIBUTION IN OPEN CHANNEL</p> <p>SHEAR DISTRIBUTION IN OPEN CHANNEL</p> |  <p>VELOCITY DISTRIBUTION IN PIPE SHEAR DISTRIBUTION IN PIPE</p> |

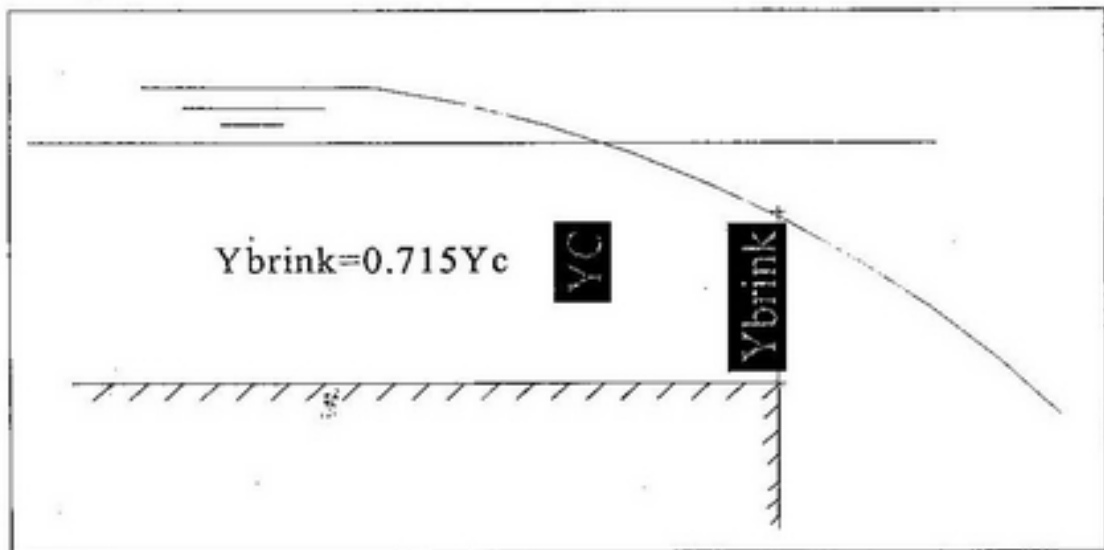
B)

-Tow conjugate depth

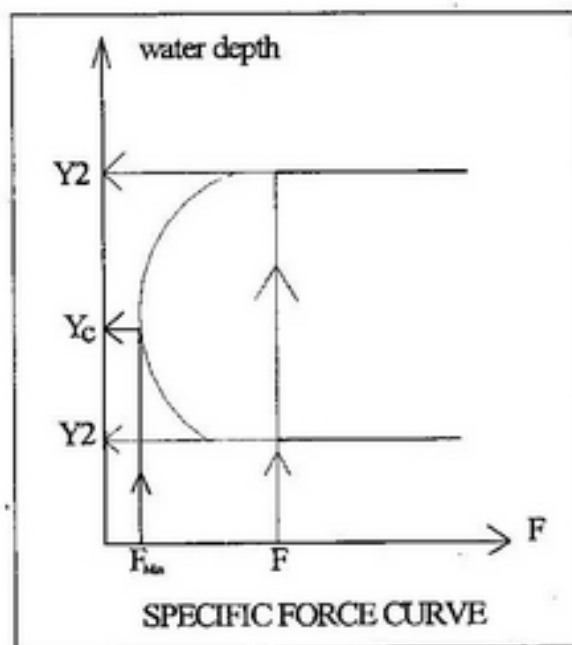
Its tow depths, h have the same specific force one of them more than critical depth and occur in sub critical flow and other less than critical depth and occur in super critical flow. And occur together.

-Control section

Its section at which water depth equal critical depth



-Specific force



Specific force diagram show relation between $(F - y)$, y_c occurs at minimum specific force. If y less than y_c flow is super critical and If y more than y_c flow is sub critical. These two depths called two conjugate depth.

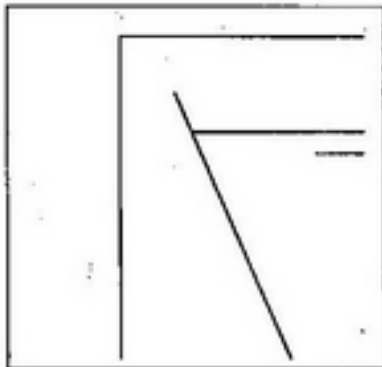
Given

YC=2.00m & So1=0.003188
So2=0.0921 & So3=0.0011262
B=4.00m & Z=2.00
Trapezoidal section

Required

- 1- tow conjugate depth
- 2- relative initial and sequent depth
- 3- jump losses and efficiency
- 4- jump length
- 5- drawing water surface profile

Solution



$$\frac{Q^2}{g} = \frac{A^3}{T}$$

$$\frac{Q^2}{9.81} = \frac{[y(b + zy)]^3}{b + 2Zy} = \frac{(2(4 + 2 \cdot 2))^3}{(4 + 2 \cdot 2 \cdot 2)}$$

$$\underline{Q = 57.886 \text{ m}^3/\text{s}}$$

$$Q = \frac{1}{n} \cdot \frac{A^{5/3}}{P^{2/3}} \cdot S^{1/2} \dots m^3/sec \dots 57.866 = \frac{1}{0.025} \cdot \frac{[y_{n2}(4+2y_{n2})]^{5/3}}{(4+2y_{n2}\sqrt{1+(2)^2})^{2/3}} \cdot (0.0003188)^{1/2}$$

$$81.022 = \frac{[y_{n2}(4+2y_{n2})]^{5/3}}{(4+2y_{n2}\sqrt{1+(2)^2})^{2/3}}$$

$$\underline{y_{n2}=4.00m}$$

$$Q = \frac{1}{n} \cdot \frac{A^{5/3}}{P^{2/3}} \cdot S^{1/2} \dots m^3/sec \dots 57.866 = \frac{1}{0.025} \cdot \frac{[y_{n2}(4+2y_{n2})]^{5/3}}{(4+2y_{n2}\sqrt{1+(2)^2})^{2/3}} \cdot (0.0921)^{1/2}$$

$$4.7669 = \frac{[y_{n2}(4+2y_{n2})]^{5/3}}{(4+2y_{n2}\sqrt{1+(2)^2})^{2/3}}$$

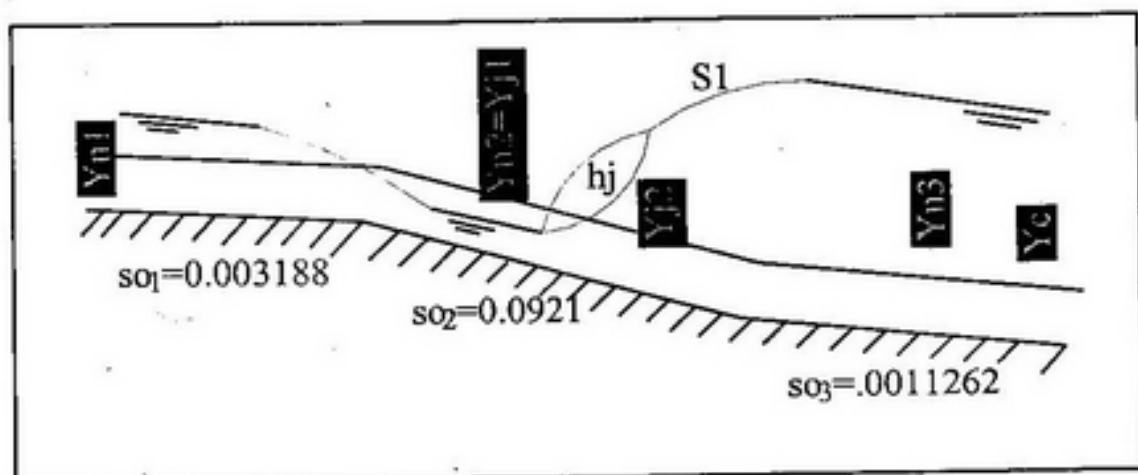
$$\underline{y_{n2}=1.00m}$$

$$Q = \frac{1}{n} \cdot \frac{A^{5/3}}{P^{2/3}} \cdot S^{1/2} \dots m^3/sec \dots 57.866 = \frac{1}{0.025} \cdot \frac{[y_{n2}(4+2y_{n2})]^{5/3}}{(4+2y_{n2}\sqrt{1+(2)^2})^{2/3}} \cdot (0.0011262)^{1/2}$$

$$43.108 = \frac{[y_{n2}(4+2y_{n2})]^{5/3}}{(4+2y_{n2}\sqrt{1+(2)^2})^{2/3}}$$

$$\underline{y_{n3}=3.00m}$$

Assume S1 occur



$$F1_1 = \frac{V_1}{\sqrt{g \cdot y_{d1}}}$$

$$V_1 = \frac{Q}{A_1} = \frac{57.866}{1.00(4 + 2 \cdot 1.00)} = 9.644 \text{ m/s}$$

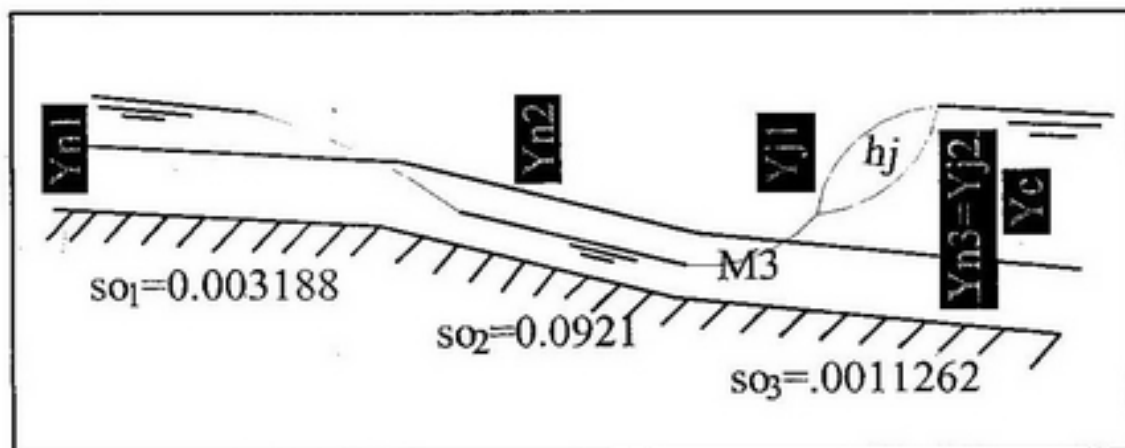
$$y_{k1} = \frac{A}{T} = \frac{1.00 \cdot (4 + 2 \cdot 1.00)}{(4 + 2 \cdot 2 \cdot 1.00)} = 0.75 \text{ m}$$

$$FI_1 = \frac{9.644}{\sqrt{9.81 \cdot 0.75}} = 3.556 > 1.00 \dots \text{super...critical..flow}$$

$$\frac{y_2}{y_1} = \frac{1}{2} (\sqrt{1 + 8FI_1^2} - 1.00)$$

$$\frac{y_2}{1.00} = \frac{1}{2} (\sqrt{1 + 8 \cdot (3.556)^2} - 1.00)$$

$$y_{j2} = 4.554 \text{ m} > y_{n2} \dots M_3 \dots \text{OCCUR}$$



$$\underline{Y_{j2}=y_{n3}=3.00 \text{ m}}$$

$$FI_2 = \frac{V_2}{\sqrt{g \cdot y_{k2}}}$$

$$V_2 = \frac{Q}{A_{21}} = \frac{57.866}{3.00(4 + 2 \cdot 3.00)} = 1.929 \text{ m/s}$$

$$y_{k2} = \frac{A_2}{T} = \frac{3.00 \cdot (4 + 2 \cdot 3.00)}{(4 + 2 \cdot 2 \cdot 3.00)} = 1.875 \text{ m}$$

$$FI_2 = \frac{1.929}{\sqrt{9.81 \cdot 1.875}} = 0.4498 < 1.00 \dots \text{sub...critical..flow}$$

$$\frac{y_1}{y_2} = \frac{1}{2}(\sqrt{1+8FI_2^2} - 1.00)$$

$$\frac{y_1}{3.00} = \frac{1}{2}(\sqrt{1+8*0.4498^2} - 1.00)$$

$$y_1 = 0.927m$$

$$E_1 = y_1 + \frac{Q^2}{2g * A_1^3} = 0.927 + \frac{(57.866)^2}{2 * 9.81 * [0.927(4 + 2 * 0.927)]^3} = 5.427$$

$$E_2 = y_2 + \frac{Q^2}{2g * A_2^3} = 3.00 + \frac{(57.866)^2}{2 * 9.81 * [3.00(4 + 2 * 3.00)]^3} = 3.019m$$

$$2 - \text{Relative Initial Depth} = \frac{y_2}{E_1} = \frac{3.00}{6.74} = 0.445$$

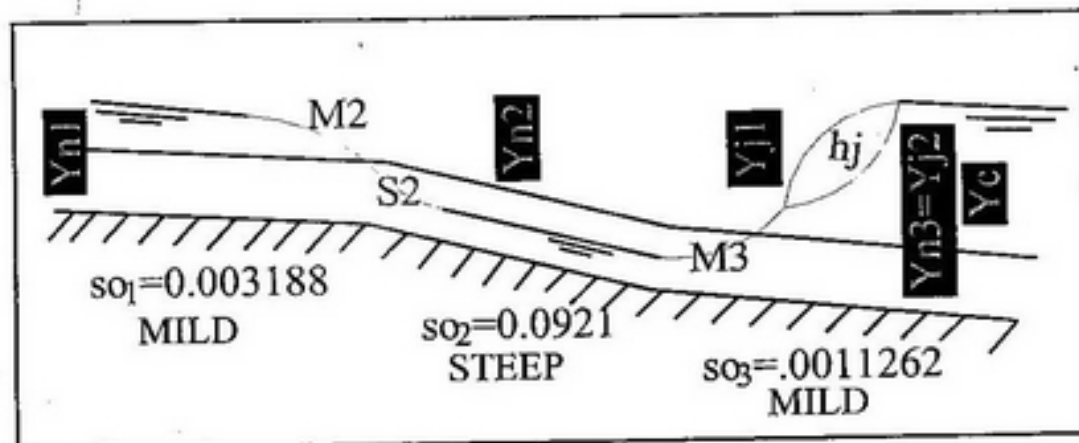
$$2 - \text{Relative sequent Depth} = \frac{y_1}{E_1} = \frac{0.927}{6.74} = 0.1375$$

$$3 - \text{head losses } h_L = E_1 - E_2 = 6.74 - 3.019 = 3.721m$$

$$3 - \text{efficiency of jump} = \frac{\gamma * Q * h_L}{75} = \frac{1000 * 57.866 * 3.721}{75} = 2870.93HP$$

$$4 - \text{Length of jump} = 5.20 * h_j = 5.20 * (3.00 - 0.926) = 10.785m$$

5-Drawing



Given

$S=0.009$

&

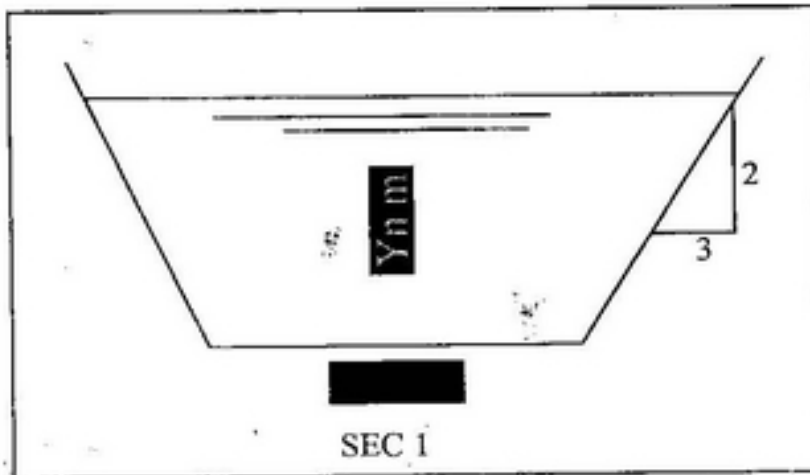
$Q=450 \text{ m}^3/\text{s}$

$n=0.025$

&

$Z=1.50$

Trapezoidal section



Required

1- $S=0.009 \text{ km/km}$
 $=0.009 \times 10^{-5} \text{ cm/km}$

$S=900 \text{ cm/km}$

2-

$$Q = \frac{1}{n} \cdot \frac{A^{5/3}}{P^{2/3}} \cdot S^{1/2} \dots \text{m}^3/\text{sec} \dots 450 = \frac{1}{0.025} \cdot \frac{[y_n(20 + 1.50y_n)]^{5/3}}{(20 + 2y_n\sqrt{1 + (1.50)^2})^{2/3}} \cdot (0.009)^{1/2}$$
$$118.585 = \frac{[y_n(20 + 1.50y_n)]^{5/3}}{(20 + 3.61y_n)^{2/3}}$$

By trial and error

$Y_n=2.83 \text{ m}$

3- $y_a = \frac{A}{T} = \frac{2.83 \cdot (20 + 1.50 \cdot 2.83)}{(20 + 2 \cdot 1.50 \cdot 2.83)} = \frac{68.6134}{28.49} = 2.408 \text{ m}$

$Y_h=2.408 \text{ m}$

$$4- FI = \frac{V}{\sqrt{g \cdot y_h}} = \frac{\left[\frac{450}{68.6134} \right]}{\left[\sqrt{9.81 \cdot 2.408} \right]} = 1.349 \dots \text{super} \dots \text{critical} \dots \text{flow}$$

FI=1.349 flow super critical

5-

$$R = \frac{A}{P} = \frac{[68.6133]}{\left[20 + 2 \cdot 2.83 \sqrt{1 + (1.50)^2} \right]} = \frac{68.6133}{30.204} = 2.272$$

$$IR = \frac{V \cdot R}{\nu} = \frac{\left(\frac{450}{68.613} \right) \cdot (2.272)}{1 \cdot 10^{-6}} = 14,900,966.29 > 2000 \dots \text{turbulent} \dots \text{flow}$$

IR=14,900,966.29 flow turbulent

Flow super critical turbulent

6-

$$\frac{Q^2}{g} = \frac{A^3}{T} \quad \frac{(450)^2}{9.81} = \frac{[y_c(b + zy_c)]^3}{b + 2zy_c} = \frac{(y_c(20 + 1.50 \cdot y_c))^3}{(20 + 2 \cdot 1.50 \cdot y_c)}$$

$$20,642.20 = \frac{(y_c(20 + 1.50 \cdot y_c))^3}{(20 + 2 \cdot 1.50 \cdot y_c)}$$

By trial and error

Y_c=3.403m > 2.83 steep slope

7-

$$y_h = \frac{A}{T} = \frac{4.50 \cdot (20 + 1.50 \cdot 4.50)}{(20 + 2 \cdot 1.50 \cdot 4.50)} = \frac{120.375}{33.50} = 3.5932m$$

$$FI = \frac{V}{\sqrt{g \cdot y_h}} = \frac{\left[\frac{450}{120.375} \right]}{\left[\sqrt{9.81 \cdot 3.5932} \right]} = 0.6296 < 1.00 \dots \text{sub} \dots \text{critical} \dots \text{flow}$$

FI=0.6296 flow sub critical

$$R = \frac{A}{P} = \frac{[120.375]}{\left[20 + 2 \cdot 4.50 \sqrt{1 + (1.50)^2} \right]} = \frac{120.375}{36.225} = 3.323$$

$$IR = \frac{V \cdot R}{\nu} = \frac{\left(\frac{450}{120.375} \right) \cdot (3.323)}{1 \cdot 10^{-6}} = 12,422,429.29 > 2000 \dots \text{turbulent} \dots \text{flow}$$

R=12,422,429.29 flow turbulent

Flow sub critical turbulent

8-

Hydraulic jump occur U/S the weir

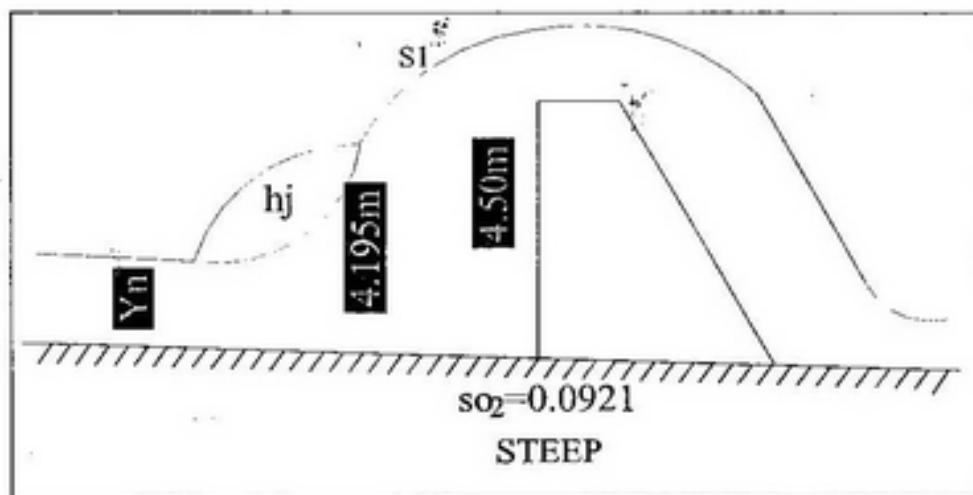
9-

$$\underline{Y_{j1} = y_n = 2.83}$$

10-

This slope is steep so

S1 occur



$$\frac{y_2}{y_1} = \frac{1}{2} (\sqrt{1 + 8FI_1^2} - 1.00)$$

$$\frac{y_2}{2.83} = \frac{1}{2} (\sqrt{1 + 8 * (1.349)^2} - 1.00)$$

$$\underline{Y_2 = 4.166m}$$

11-

This slope is steep

12-

Water surface profile U/S the weir

13-

$$E_1 = y_1 + \frac{Q^2}{2g * A_1^2} = 4.195 + \frac{(450)^2}{2 * 9.81 * [4.195(20 + 1.50 * 4.195)]^2} = 5.0435$$

$$\underline{E_1 = 5.0435m}$$

14-

$$E_2 = y_2 + \frac{Q^2}{2g * A_2^2} = 4.50 + \frac{(450)^2}{2 * 9.81 * [4.50 * (20 + 1.50 * 4.50)]^2} = 5.212m$$

$$\underline{E_2 = 5.212m}$$

15-

$$\Delta E = E_2 - E_1 = 5.212 - 5.0435 = 0.1685m$$

$$\Delta E = 0.1685m$$

16-

$$Q = \frac{1}{n} \cdot \frac{A^{5/2}}{P^{3/2}} \cdot S^{1/2} \dots m^3/sec \dots 450 = \frac{1}{0.025} \cdot \frac{[y_n(20 + 1.50y_{n2})]^{5/2}}{(20 + 2y_n\sqrt{1 + (1.50)^2})^{3/2}} \cdot (SO_1)^{1/2}$$

$$450 = \frac{1}{0.025} \cdot \frac{[4.195(20 + 1.50 \cdot 4.195)]^{5/2}}{(20 + 2 \cdot 4.195 \cdot \sqrt{1 + (1.50)^2})^{3/2}} \cdot (SO_1)^{1/2}$$

$$450 = \frac{1}{0.025} \cdot \frac{[110.29]^{5/2}}{[35.125]^{3/2}} \cdot (SO_1)^{1/2}$$

$$SO_1 = 2.262 \cdot 10^{-3}$$

$$Q = \frac{1}{n} \cdot \frac{A^{5/2}}{P^{3/2}} \cdot S^{1/2} \dots m^3/sec \dots 450 = \frac{1}{0.025} \cdot \frac{[y_n(20 + 1.50y_{n2})]^{5/2}}{(20 + 2y_n\sqrt{1 + (1.50)^2})^{3/2}} \cdot (SO_2)^{1/2}$$

$$450 = \frac{1}{0.025} \cdot \frac{[4.50(20 + 1.50 \cdot 4.50)]^{5/2}}{(20 + 2 \cdot 4.50 \cdot \sqrt{1 + (1.50)^2})^{3/2}} \cdot (SO_2)^{1/2}$$

$$450 = \frac{1}{0.025} \cdot \frac{[120.375]^{5/2}}{[36.225]^{3/2}} \cdot (SO_2)^{1/2}$$

$$SO_2 = 1.7614 \cdot 10^{-3}$$

$$\begin{aligned} SE_{AVE} &= (SO_1 + SO_2)/2 \\ &= (2.262 \cdot 10^{-3} + 1.7614 \cdot 10^{-3})/2 \\ &= 2.0117 \cdot 10^{-3} \end{aligned}$$

$$SE_{AVE} = 2.0117 \cdot 10^{-3}$$

17-

$$\begin{aligned} \Delta S &= S_0 - SE_{AVE} \\ &= 6.9983 - 2.0117 \cdot 10^{-3} \\ &= 6.9983 \cdot 10^{-3} \end{aligned}$$

$$\Delta x = \frac{\Delta E}{\Delta S} = \frac{0.1685}{6.9983 \cdot 10^{-3}} = 24.078$$

$$\Delta X = 24.00 \text{ m}$$

18-

$$K = \frac{1}{n} \cdot \frac{A^{\frac{5}{3}}}{P^{\frac{2}{3}}} \dots m^3/sec \dots K = \frac{1}{0.025} \cdot \frac{[2.83(20 + 1.50 \cdot 2.83)]^{\frac{5}{3}}}{(20 + 2 \cdot 2.83 \sqrt{1 + (1.50)^2})^{\frac{2}{3}}} = 4742.79 m^3/sec$$

$$K = 4742.79 m^3/S$$

19 -

$$A = [3.403(20 + 1.50 \cdot 3.403)] = 85.43 m^2$$

$$y_h = \frac{A}{T} = \frac{85.43}{(20 + 2 \cdot 1.50 \cdot 3.403)} = \frac{85.43}{30.209} = 2.828 m$$

$$Z = A \sqrt{y_h} = 85.43 \cdot \sqrt{2.828} = 143.664$$

Or

$$Z = \sqrt{\frac{Q^2}{g}} = \sqrt{\frac{430^2}{9.81}} = 143.664 m^{2.5}$$

$$Z = 143.664 m^{2.5}$$

| NO | ١ | ٢ | ٣ | ٤ | ٥ | ٦ | ٧ | ٨ | ٩ | ١٠ | ١١ | ١٢ | ١٣ | ١٤ | ١٥ | ١٦ | ١٧ | ١٨ | ١٩ |
|--------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|
| answer | C | b | a | c | b | b | a | a | a | a | b | a | a | a | a | a | a | a | c |